

# Duration of urination does not change with body size

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Many urological studies rely on models of animals, such as rats and pigs, but their relation to the human urinary system is poorly understood. Here, we elucidate the hydrodynamics of urination across five orders of magnitude in body mass. Using high-speed videography and flow-rate measurement obtained at Zoo Atlanta, we discover that all mammals above 3 kg in weight empty their bladders over nearly constant duration of  $21 \pm 13$  s. This feat is possible, because larger animals have longer urethras and thus, higher gravitational force and higher flow speed. Smaller mammals are challenged during urination by high viscous and capillary forces that limit their urine to single drops. Our findings reveal that the urethra is a flow-enhancing device, enabling the urinary system to be scaled up by a factor of 3,600 in volume without compromising its function. This study may help to diagnose urinary problems in animals as well as inspire the design of scalable hydrodynamic systems based on those in nature.

urology | allometry | scaling | Bernoulli's principle

Medical and veterinary urology often relies on simple, non-invasive methods to characterize the health of the urinary system (1, 2). One of the most easily measured characteristics of the urinary system is its flow rate (3), changes in which may be used to diagnose urinary problems. The expanding prostates of aging males may constrict the urethra, decreasing urine flow rate (4). Obesity may increase abdominal pressure, causing incontinence (5). Studies of these ailments and others often involve animal subjects of a range of sizes (6). A study of urination in zero gravity involved a rat suspended on two legs for long periods of time (7), whereas other studies involve mice (8), dogs (1), and pigs (9). Despite the wide range of animals used in urological studies, the consequences of body size on urination remain poorly understood.

The bladder serves a number of functions, as reviewed by Bentley (10). In desert animals, the bladder stores water to be retrieved at a time of need. In mammals, the bladder acts as a waterproof reservoir to be emptied at a time of convenience. This control of urine enables animals to keep their homes sanitary and themselves inconspicuous to predators. Stored urine may even be used in defense, which one knows from handling rodents and pets.

Several misconceptions in urology have important repercussions in the interpretation of healthy bladder function. For instance, several investigators state that urinary flow is driven entirely by bladder pressure. Consequently, their modeling of the bladder neglects gravitational forces (11–13). Others, such as Martin and Hillman (14), contend that urinary flow is driven by a combination of both gravity and bladder pressure. In this study, we elucidate the hydrodynamics of urination across animal size, showing the effects of gravity increase with increasing body size.

## Results

**In Vivo Experiments.** We filmed the urination of 16 animals and obtained 28 videos of urination from YouTube, listed in *SI Appendix*. Movies S1–S4 show that urination style is strongly dependent on animal size. Here, we define an animal as large if it is heavier than 3 kg and an animal as small if it is lighter than 1 kg. Large animals, from dogs to elephants, produce jets and sheets of urine, which are shown in Fig. 1*A–D*. Small animals, including rodents, bats, and juveniles of many mammalian species, cannot

generate jets. Instead, they urinate using a series of drops, which is shown by the 0.03-kg lesser dog-faced fruit bat and the 0.3-kg rat in Fig. 2*A–C*, respectively.

Fig. 1*H* shows the urination time for 32 animals across six orders of magnitude of body mass from 0.03 to 8,000 kg. Despite this wide range in mass, urination time remains constant,  $T = 21 \pm 13$  s ( $n = 32$ ), for all animals heavier than 3 kg. This invariance is noteworthy, considering that an elephant's bladder, at 18 L, is nearly 3,600 times larger in volume than a cat's bladder at 5 mL. Using the method of least squares, we fit the data to a clear scaling law shown by the dashed line:  $T \sim M^{0.13}$  (Fig. 1*H*).

For small animals, urination is a high-speed event of 0.01- to 2-s duration and therefore, quite different from the behavior of the large animals observed that urinate for 21 s. Fig. 1*H* shows urination time across 11 small animals, including one bat, five rats, and five mice. Their body masses ranged from 0.03 to 0.3 kg. The large error bar for the rats is caused by bladder fullness varying across individuals. Fig. 2*D* shows the time course of the urine drop's radius measured by image analysis of high-speed video of a rat. To rationalize the striking differences between large and small animals, we turn to mathematical modeling of the urinary system.

**Modeling Assumptions.** Urination may be simply described mathematically. Fig. 1*E* shows a schematic of the urinary system, consisting of a bladder of volume  $V$  and the urethra, which is assumed to be a straight vertical pipe of length  $L$  and diameter  $D$ . We assume that the urethra has such a thin wall that its internal and external diameters are equal. Urination begins when the smooth muscles of the bladder pressurize the urine to  $P_{\text{bladder}}$ , measured relative to atmospheric pressure. After an initial transient of duration that depends on the system size, a steady flow of speed  $u$  is generated.

Previous medical and veterinary studies, particularly cystometry and ultrasonography, report substantial data on the anatomy, pressure, and flow rate of the urinary system. Fig. 3 shows urethral length (8, 15–25) and diameter (15, 24–34), flow rate (35–42), bladder capacity (25, 43–49), and bladder pressure (1, 35, 39, 40, 43, 46, 50) for over 100 individuals across 13 species.

## Significance

Animals eject fluids for waste elimination, communication, and defense from predators. These diverse systems all rely on the fundamental principles of fluid mechanics, which we use to predict urination duration across a wide range of mammals. In this study, we report a mathematical model that clarifies misconceptions in urology and unifies the results from 41 independent urological and anatomical studies. The theoretical framework presented may be extended to study fluid ejection from animals, a universal phenomenon that has received little attention.

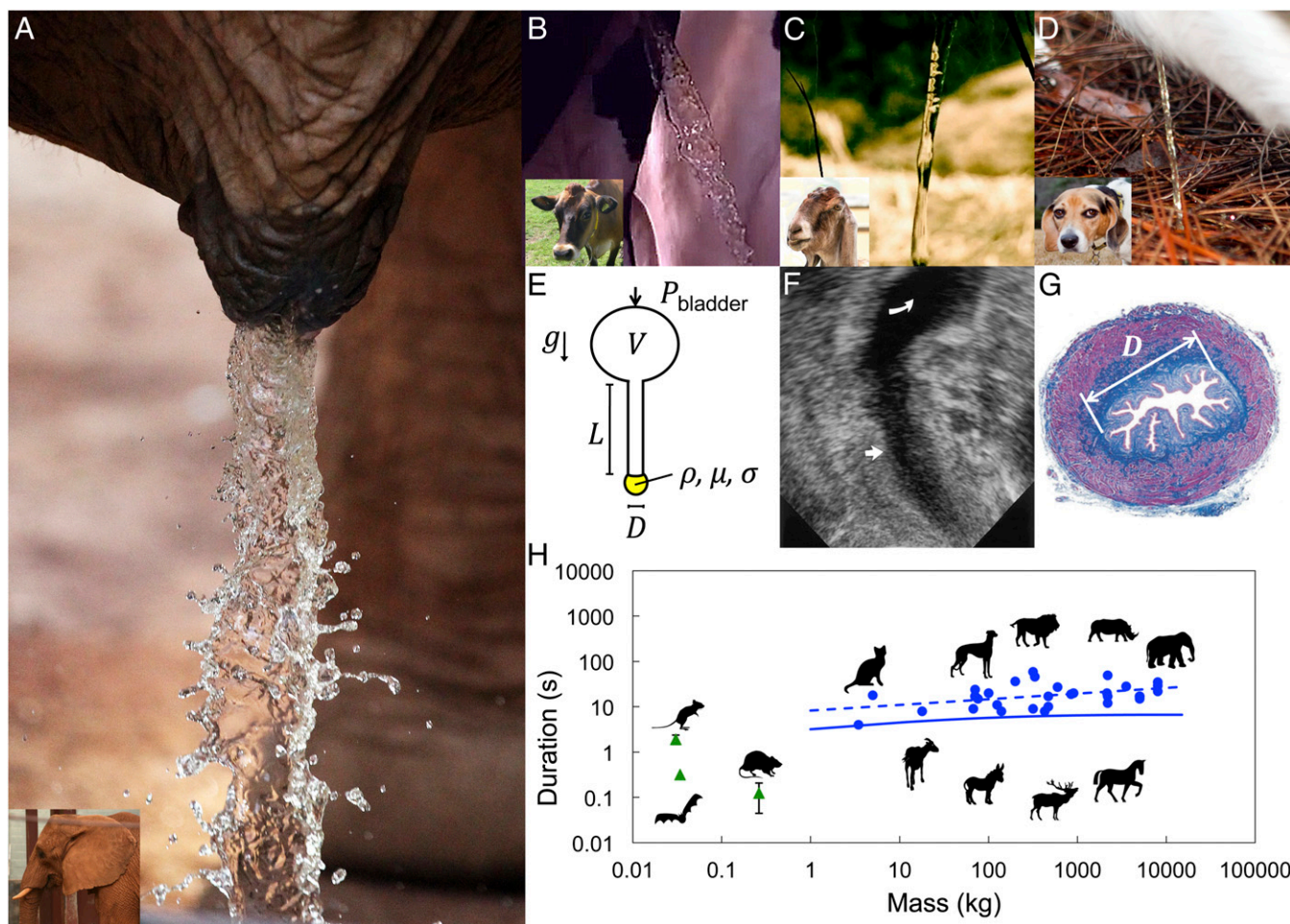
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**Fig. 1.** Jetting urination by large animals, including (A) elephant, (B) cow, (C) goat, and (D) dog. *Inset* of cow is reprinted from the public domain and cited in *SI Appendix*. (E) Schematic of the urinary system. (F) Ultrasound image of the bladder and urethra of a female human. The straight arrow indicates the urethra, and the curved arrow indicates the bladder. Reproduced with permission from ref. 20, (Copyright 2005, Radiological Society of North America). (G) Transverse histological sections of the urethra from a female pig. Reproduced with permission from ref. 9, (Copyright 2001, Elsevier). (H) The relationship between body mass and urination time.

Table 1 shows the corresponding allometric relationships to be used in numerical predictions for flow rate and urination time.

We begin by showing that the urinary system is isometric (i.e., it has constant proportions across animal size). Fig. 3A shows the relation between body mass  $M$  and urethral dimensions (length  $L$  and diameter  $D$ ). As shown by the nearly parallel trends for  $L$  and  $D$  ( $L = 35M^{0.43}$  and  $D = 2M^{0.39}$ ), the aspect ratio of the urethra is 18. Moreover, the exponents are close to the expected isometric scaling of  $M^{1/3}$ . Fig. 3B shows the relationship between body mass and bladder capacity. The bladder's capacity is  $V \sim M^{0.97}$ , and the exponent of near unity indicates isometry.

In ultrasonic imaging (Fig. 1F), the urethra appears circular (20). However, in histology (Fig. 1G), the urethra is clearly corrugated, which decreases its cross-sectional area (9). The presence of such corrugation has been verified in studies in which flow is driven through the urethra (51, 52), although the precise shape has been too difficult to measure. We proceed by using image analysis to measure cross-sectional area  $A$  from urethral histological diagrams of dead animals in the absence of flow (9, 53, 54). We define a shape factor  $\alpha = 4A/\pi D^2$ , which relates the urethral cross-sectional area with respect to that of a cylinder of diameter  $D$ . Fig. 3C shows the shape factor  $\alpha = 0.2 \pm 0.05$  ( $n = 5$ ) for which the corrected cross-sectional area is 20% of the original area considered.

This shape factor is nearly constant across species and body mass and consistent with the value of 0.17 found by Wheeler et al. (55).

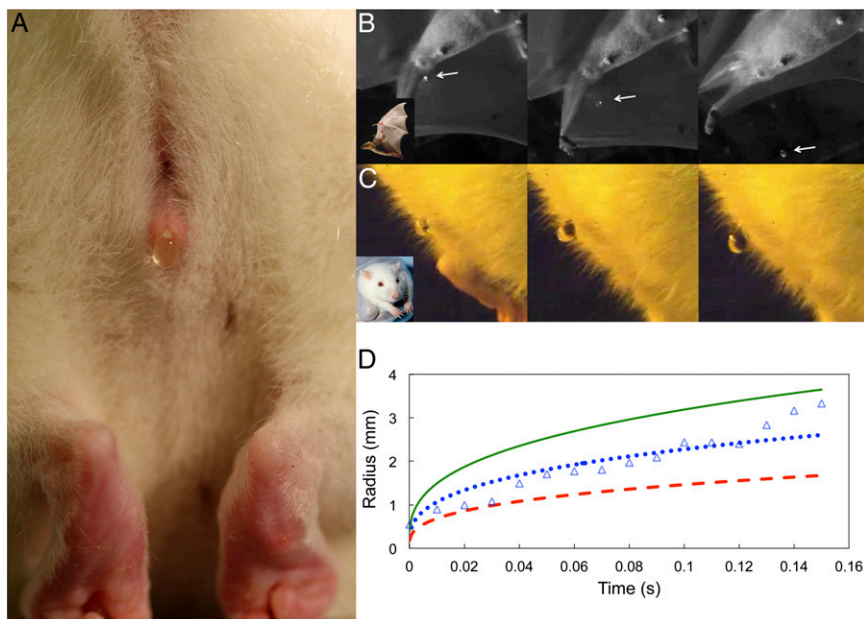
Peak bladder pressure is difficult to measure *in vivo*, and instead, it is estimated using pressure transducers placed within the bladders of anesthetized animals. Pressure is measured when the bladder is filled to capacity by the injection of fluid. This technique yields a nearly constant bladder pressure across animal size:  $P_{\text{bladder}} = 5.2 \pm 0.86$  kPa ( $n = 8$ ), which is shown in Fig. 3D. The constancy of bladder pressure at 5.2 kPa is consistent with other systems in the body. One prominent example is the respiratory system, which generates pressures of 10 kPa for animals spanning from a mosquito to an elephant (56).

**Steady-State Equation of Urine Flow.** We model the flow as steady state and the urine as an incompressible fluid of density  $\rho$ , viscosity  $\mu$ , and surface tension  $\sigma$ . The energy equation relates the pressures involved, each of which has units of energy per cross-sectional area of the urethra per unit length down the urethra:

$$P_{\text{bladder}} + P_{\text{gravity}} = P_{\text{inertia}} + P_{\text{viscosity}} + P_{\text{capillary}}. \quad [1]$$

Each term in Eq. 1 may be written simply by considering the pressure difference between the entrance and exit of the





**Fig. 2.** Dripping urination by small animals. (A) A rat's excreted urine drop. (B) A urine drop released by the lesser dog-faced fruit bat *Cynopterus brachyotis*. Courtesy of Kenny Breuer and Sharon Swartz. (C) A rat's urine drop grows with time. *Inset* is reprinted from the public domain and cited in *SI Appendix*. (D) Time course of the drop radii of the rat (triangles) along with prediction from our model (blue dotted line,  $\alpha = 0.5$ ; green solid line,  $\alpha = 1$ ; red dashed line,  $\alpha = 0.2$ ).

urethra. The combination of bladder and hydrostatic pressure drives urine flow. Bladder pressure  $P_{\text{bladder}}$  is a constant given in Fig. 3D. We do not model the time-varying height in the bladder, because bladders vary greatly in shape (57). Thus, hydrostatic pressure scales with urethral length:  $P_{\text{gravity}} \sim \rho g L$ , where  $g$  is the acceleration of gravity. Dynamic pressure  $P_{\text{inertia}}$  scales as  $\rho u^2/2$  and is associated with the inertia of the flow.

The viscous pressure drop in a long cylindrical pipe is given by the Darcy–Weisbach equation (58):  $P_{\text{viscosity}} = f_D(\text{Re})\rho L u^2/2\alpha D$ . We use  $\sqrt{\alpha}D$  as the effective diameter of the pipe to keep the cross-sectional area of the pipe consistent with experiments. The Darcy friction factor  $f_D$  is a function of the Reynolds number  $\text{Re} = \rho u D/\mu$ , such that  $f_D(\text{Re}) = 64/\text{Re}$  for laminar flow and  $f_D(\text{Re}) = 0.316/\text{Re}^{1/4}$  for turbulent flow ( $10^4 < \text{Re} < 10^5$ ). Drops generated from an orifice of effective diameter  $\sqrt{\alpha}D$  experience a capillary force (59) of  $P_{\text{capillary}} = 4\sigma/\sqrt{\alpha}D$ . Substituting these terms into Eq. 1, we arrive at

$$P_{\text{bladder}} + \rho g L = \frac{\rho u^2}{2} + f_D(\text{Re}) \frac{\rho L u^2}{2\alpha D} + \frac{4\sigma}{\sqrt{\alpha}D}. \quad [2]$$

The relative magnitudes of the five pressures enumerated in Eq. 2 are prescribed by six dimensionless groups, including the aforementioned Reynolds number and Darcy friction factor and well-known Froude  $\text{Fr} = u/\sqrt{gL}$  and Bond  $\text{Bo} = \rho g D^2/\sigma$  numbers (60) as well as dimensionless groups pertaining to the urinary system, the urethra aspect ratio  $\text{As} = D/L$ , and pressure ratio  $\text{Pb} = P_{\text{bladder}}/\rho g L$ . Using these definitions, we nondimensionalize Eq. 2 to arrive at

$$\text{Pb} + 1 = \frac{\text{Fr}^2}{2} + f_D(\text{Re}) \frac{\text{Fr}^2}{2\alpha \text{As}} + \frac{4\text{As}}{\sqrt{\alpha}\text{Bo}}. \quad [3]$$

In the following sections, we solve Eq. 3 in the limits of large and small animals.

In *SI Appendix*, we apply a variation of the Washburn law (61) to show that the steady-state model given in Eq. 2 is accurate for most animals. Animals lighter than 100 kg achieve 90% of their flow velocity within 4 s; however, for animals such as elephants, the transient phase can be substantial. For

our derivations here, however, we assume that the transient phase is negligible.

**Large Animals Urinate for Constant Duration.** Bladder pressure, gravity, and inertia are dominant for large animals, which can be shown by consideration of the dimensionless groups in *SI Appendix*. Eq. 2 reduces to

$$P_{\text{bladder}} + \rho g L = \frac{\rho u^2}{2}. \quad [4]$$

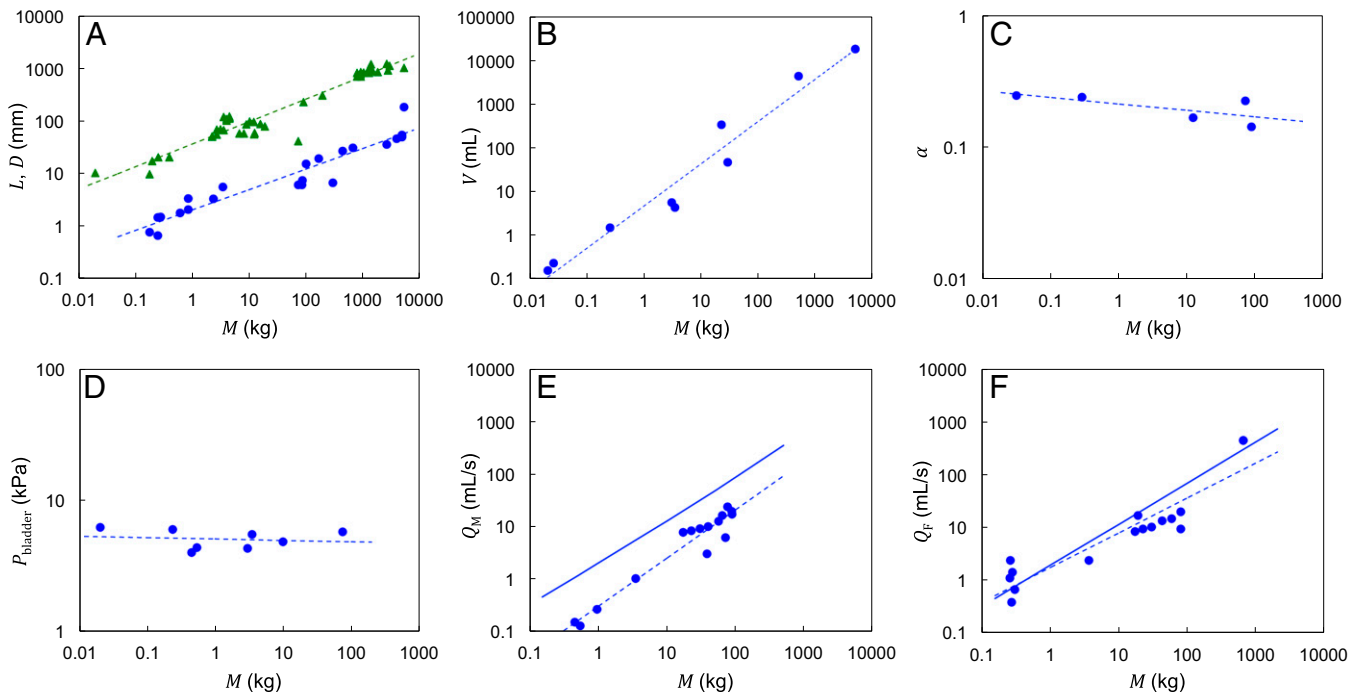
The urination time  $T$ , the time to completely empty the bladder, may be written as the ratio of bladder capacity to time-averaged flow rate,  $T = V/Q$ . We define the flow rate as  $Q = uA$ , where  $A = \alpha\pi D^2/4$  is the cross-sectional area of the urethra. Using Eq. 4 to substitute for flow speed yields

$$T = \frac{4V}{\alpha\pi D^2 \left( \frac{2P_{\text{bladder}}}{\rho} + 2gL \right)^{1/2}}. \quad [5]$$

By isometry, bladder capacity  $V \sim M$  and urethral length and diameter both scale with  $M^{1/3}$ ; substitution of these scalings into Eq. 5 yields urination time  $T \sim M^{1/6} \approx M^{0.16}$  in the limit of increasing body mass. Agreement between predicted and measured scaling exponents is very good (0.13 compared with 0.16). We, thus, conclude that our scaling has captured the observed invariance in urination time.

We go beyond a simple scaling by substituting the measured allometric relationships from Table 1 for  $L$ ,  $D$ ,  $\alpha$ ,  $V$ , and  $P_{\text{bladder}}$  into Eq. 5, yielding a numerical prediction for urination time. This prediction (Fig. 1H, solid line) is shown compared with experimental values (Fig. 1H, dashed line). The general trend is captured quite well. We note that numerical values are under-predicted by a factor of three across animal masses, likely because of the angle and cross-section of the urethra in vivo.

How can an elephant empty its bladder as quickly as a cat? Larger animals have longer urethras and therefore, greater hydrostatic pressure driving flow. Greater pressures lead to higher flow rates, enabling the substantial bladders of larger animals to be emptied in the same duration as those of their much smaller counterparts.



**Fig. 3.** The relation between body mass  $M$  and properties of the urinary system. (A) Urethral length  $L$  (green triangles) and diameter  $D$  (blue circles). (B) Bladder capacity  $V$ . (C) Shape factor  $\alpha$  associated with the urethral cross-section. (D) Bladder pressure  $P_{\text{bladder}}$ . (E) Flow rate of males. (F) Flow rate of females. Symbols represent experimental measurements, dashed lines represent best fits to the data, and solid lines represent predictions from our model.

Our model provides a consistent physical picture on consideration of flow rate. Combining Eq. 4 and the definition of flow rate ( $Q = uA$ ) yields

$$Q = \frac{\alpha \pi D^2}{4} \left( \frac{2P_{\text{bladder}}}{\rho} + 2gL \right)^{1/2}. \quad [6]$$

Our model gives insight into the distinct flow-rate scalings observed for both male and female mammals. Male mammals generally stand on four legs and have a penis that extends downward, enabling them to urinate vertically. Assuming isometry ( $D \sim M^{1/3}$  and  $L \sim M^{1/3}$ ), flow rate scales as  $Q \sim M^{5/6} \approx M^{0.83}$  in the limit of large body mass. This predicted exponent is within 10% of the observed scaling for males:  $Q_M \sim M^{0.92}$ . By substituting the allometric relations from Table 1 into Eq. 6, we compute a numerical prediction for flow rate (Fig. 3E, solid line) that is five times higher than experimental flow rates (Fig. 3E, dashed line). This overprediction is roughly consistent with our underprediction for urination time.

Female mammals have anatomy such that the urethral exit is near the anus: thus, many female animals urinate horizontally. The scaling of Eq. 6 without the gravitational term is  $Q \sim M^{2/3} \approx M^{0.67}$ , and the exponent is in correspondence to that found in our experiments for females:  $Q_F \sim M^{0.66}$ . Substituting allometric relations from Table 1 yields a numerical prediction (Fig. 3F, solid line) that remains in good agreement with experiments.

**Small Animals Urinate Quickly and for Constant Duration.** Bladder pressure, viscous pressure, and capillary pressure are dominant for small animals, which is shown by the associated dimensionless groups in *SI Appendix*. In this limit, Eq. 2 reduces to

$$P_{\text{bladder}} = \frac{\rho u^2}{2} + \frac{32\mu Lu}{\alpha D^2} + \frac{4\sigma}{\sqrt{\alpha D}}, \quad [7]$$

which we solve numerically for flow speed  $u$ . To predict the flow speed of a rat, inputs to this equation include the rat's bladder

pressures and urethral anatomy (15, 16, 50) ( $P_{\text{bladder}} = 6.03$  kPa,  $L = 20$  mm,  $D = 0.8$  mm).

To determine urination time, we turn to the dynamics of drop filling. A spherical drop is filled by the influx of urine,  $Q = \alpha \pi D^2 u / 4$ . By conservation of mass,  $dV_{\text{drop}}/dt = Q$ , a first-order differential equation that may be easily integrated to obtain the drop volume  $V(t)$ . We assume that the initial drop corresponds to a sphere of the same diameter as the urethra,  $\sqrt{\alpha}D$ . Thus, the radius of the spherical urine drop may be written

$$R(t) = \left( \frac{\alpha^3 D^3}{8} + \frac{3\alpha D^2 u t}{16} \right)^{1/3}. \quad [8]$$

Combining Eq. 8 and the numerical solution for Eq. 7, we compute the time course of the drop radius. This prediction is compared with experimental values in Fig. 2D. We find that the prediction is highly sensitive to the value of  $\alpha$ . Without consideration of the corrugated cross-section, a prediction of  $\alpha = 1$  (Fig. 2D, green solid line) yields a flow rate that is too high. Using the shape factor  $\alpha = 0.2$  (Fig. 2D, red dashed line), our model predicts a flow speed of  $u = 1.2$  m/s, which fits the data fairly well. Using nonlinear least-squares fitting in Matlab, the best fit to the experimental data yields an intermediate value of  $\alpha = 0.5$  (Fig. 2D, blue dotted line).

The drop does not grow without limit but falls when its gravitational force, scaling as  $4\pi R_f^3 \rho g / 3$ , overcomes its attaching capillary force to the urethra, scaling as  $\pi \sqrt{\alpha} D \sigma$ . Equating these two forces yields the final drop radius before detachment,

$$R_f = \left( \frac{3\sigma \sqrt{\alpha} D}{4\rho g} \right)^{1/3}, \quad [9]$$

which does a fair job of predicting the drop size. We predict drop radii for rats and mice of 1.3 and 1.1 mm, respectively, which are two times as large as experimental values of  $2.0 \pm 0.1$  ( $n = 5$ ) and

**Table 1. Measured allometric relationships for the urinary system of animals**

	Variable	Unit	Best fit	$R^2$	$N$
Duration of urination	$T$	s	$8.2 M^{0.13}$	0.2	32
Urethral length	$L$	mm	$35 M^{0.43}$	0.9	47
Urethral diameter	$D$	mm	$2.0 M^{0.39}$	0.9	22
Shape factor	$\alpha$	—	$0.2 M^{-0.05}$	0.5	5
Bladder capacity	$V$	mL	$4.6 M^{0.97}$	0.9	9
Bladder pressure	$P_{\text{bladder}}$	kPa	$5.2 M^{-0.01}$	0.02	8
Flow rate for females	$Q_F$	mL/s	$1.8 M^{0.66}$	0.9	16
Flow rate for males	$Q_M$	mL/s	$0.3 M^{0.92}$	0.9	15

Body mass  $M$  given in kilograms. Duration of urination corresponds to animals heavier than 3 kg. Urethral length and diameter, shape factor, bladder capacity, bladder pressure, and flow rates correspond to animals heavier than 0.02 kg.

$2.2 \pm 0.4$  mm ( $n = 5$ ), respectively. We suspect this difference is caused by our underestimation of urethral perimeter at the exit. For such a large drop to remain attached, we require the attachment diameter to be larger by a factor of two, which is quite possible, because the urethral exit is elliptical.

Substituting Eq. 9 into Eq. 8, the time to eject one drop may be written

$$T_{\text{drop}} = \frac{16\sqrt{\alpha}D}{3u} \left( \frac{3 \cos \theta}{4\alpha^3 \text{Bo}} - \frac{1}{8} \right) \approx \frac{4D \cos \theta}{\sqrt{\alpha} \text{Bo}} \frac{1}{u} \quad [10]$$

The predictions of maximum drop size and time to fall are in excellent correspondence with observed values for rats and mice. Using Eq. 10, we predict drop falling times of 0.05 and 0.15 s for rats and mice, respectively, which are nearly identical to experimental values of  $0.06 \pm 0.05$  ( $n = 5$ ) and  $0.14 \pm 0.1$  s ( $n = 14$ ), respectively.

A scaling for urine duration for small animals is not straightforward because of the nonlinearity of Eq. 7. We conduct a scaling analysis in the limit of decreasing animal size for which the Reynolds number approaches zero. Because of isometry,  $V \sim M$  and  $D \sim M^{1/3}$ . Rewriting Eq. 7 at low Reynolds number, we have  $u \sim D$ , and therefore, the time to eject one drop from Eq. 10 scales as  $T_{\text{drop}} \sim \text{Bo}^{-1} \sim M^{-2/3}$ . Using Eq. 9, the final drop size is  $R_f \sim D \sim M^{1/3}$ . By conservation of mass, a full bladder of volume  $V$  can produce  $N$  spherical drops, where  $N = 3V/4\pi R_f^3 \sim M^{2/3}$ . Thus, the urination time for small animals  $T = NT_{\text{drop}}$  is constant and therefore, independent of animal size. This prediction indicates that small animals urinate for different durations than large animals, which is in correspondence with experiments. Our experiments indicate that mammals of mass 0.03–0.3 kg urinate for durations of 0.1–2 s. We have insufficient range of masses for small animals to conclude our prediction that urination time is constant in this regime.

The model yields insight into the challenges faced by small animals. In Eq. 7, flow speed is positive only if  $P_{\text{bladder}}\sqrt{\alpha}D \geq 4\sigma$ , where  $\sigma$  is the surface tension of urine, which for humans is comparable with the surface tension of water (62). Thus, we predict that the smallest urethra to expel urine has a diameter of  $4\sigma/\sqrt{\alpha}P_{\text{bladder}} \sim 0.1$  mm. According to our allometric trends, the smallest animal that can urinate independently corresponds to a body mass of 0.8 g and urethral length of 1.7 mm. This mass corresponds to that of altricial mice (0.5–3 g), which are dependent on their mother's licking of excreted urine drops (63).

## Discussion

The urinary system works effectively across a range of length scales. This robustness is caused by the hydrodynamic contribution of the

urethra. In the medical literature, the function of the urethra was previously unknown. It was simply defined as a conduit between bladder and genitals. In this study, we find that the urethra is analogous to Pascal's Barrel: by providing a water-tight pipe to direct urine downward, the urethra increases the gravitational force acting on urine and therefore, the rate at which urine is expelled from the body. Thus, the urethra is critical to the bladder's ability to empty quickly as the system is scaled up. Engineers may apply this result to design a system of pipes and reservoirs for which the drainage time does not depend on system size. This concept of a scalable hydrodynamic system may be used in the design of portable reservoirs, such as water towers, water backpacks, and storage tanks.

Why is urination time 21 s, and why is this time constant across animal sizes? The numerical value of 21 s arises from the underlying physics involving the physical properties of urine as well as the dimensions of the urinary system. Our model shows that differences in bladder capacity are offset by differences in flow rate, resulting in a bladder emptying time that does not change with system size. Such invariance has been observed in a number of other systems. Examples include the height of a jump (64) and the number of heartbeats in a lifetime (65). Many of these examples arise from some aspect of isometry, such as with our system.

From a biological perspective, the invariance of urination time suggests its low functional significance. Because bladder volume is 4.6 mL/kg body mass and daily urine voided is 26 mL/kg body mass (66), mammals urinate 5.6 times/d. Because the time to urinate once is 21 s, the daily urination time is 2 min, which can be translated to 0.2% of an animal's day, a negligible portion compared with other daily activities, such as eating and sleeping, for which most animals take care to avoid predation. Thus, urination time likely does not influence animal fitness. The geometry of the urethra, however, may play a role in other activities of high functional significance, such as ejaculation.

In our study, we found that urination time is highly sensitive to urethral cross-section. This dependency is particularly high for small animals for which urine flow is resisted by capillary and viscous forces, which scale with the perimeter of the urethra. More accurate predictions for small animals require measurements of the urethral exit perimeter and the urethral cross-section, which is known to vary with distance down the urethra (67). Current models of noncircular pipe flow are not applicable, because they only account for infinitesimal corrugations (68). Additional mathematical techniques as well as accurate urethral measurements are needed to increase correspondence with experiments.

## Materials and Methods

We filmed urination of animals using both Sony HDR-XR200 and high-speed cameras (Vision Research v210 and Miro 4). The masses of animals are taken from annual veterinary procedures or measured using an analytical balance. Flow rate  $Q$  is measured by simultaneous high-speed videography and manual urine collection using containers of appropriate size and shape. We use the open-source software Tracker to measure the time course of the radius of urine drops produced by rats and mice.

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